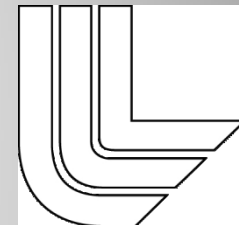


High speed imaging of metal additive manufacturing processes



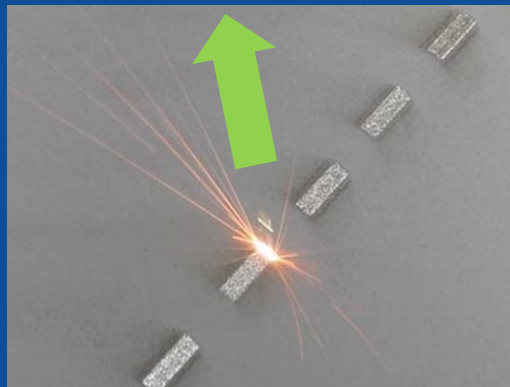
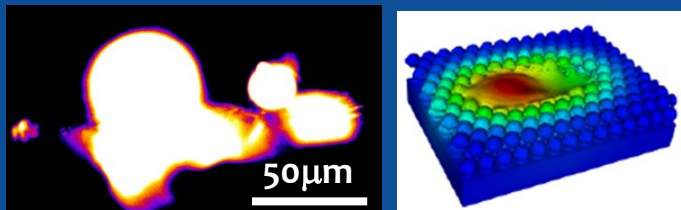
Ibo Matthews,^{1,3} Alexander Rubenchik,³ Saad Khairallah² and Gabe Guss^{2,3}

1-Physical & Life Sciences Directorate

2-Engineering Directorate

3-National Ignition Facility & Photon Science Directorate

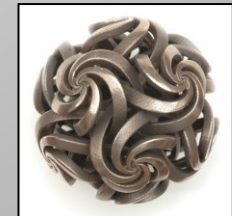
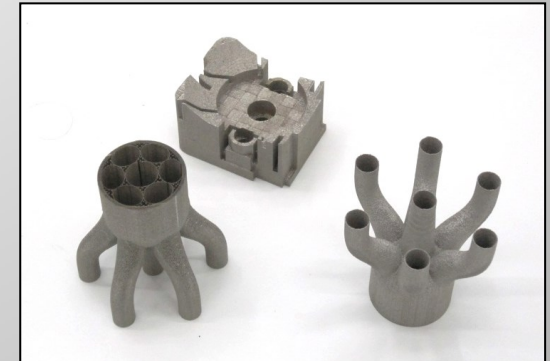
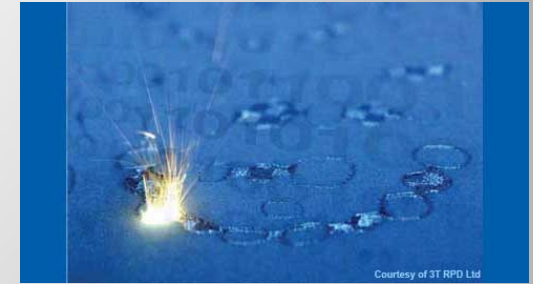
Lawrence Livermore National Laboratory, Livermore CA 94550



This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under Contract DE-AC52-07NA27344. Information management release number LLNL-PRES-670542.

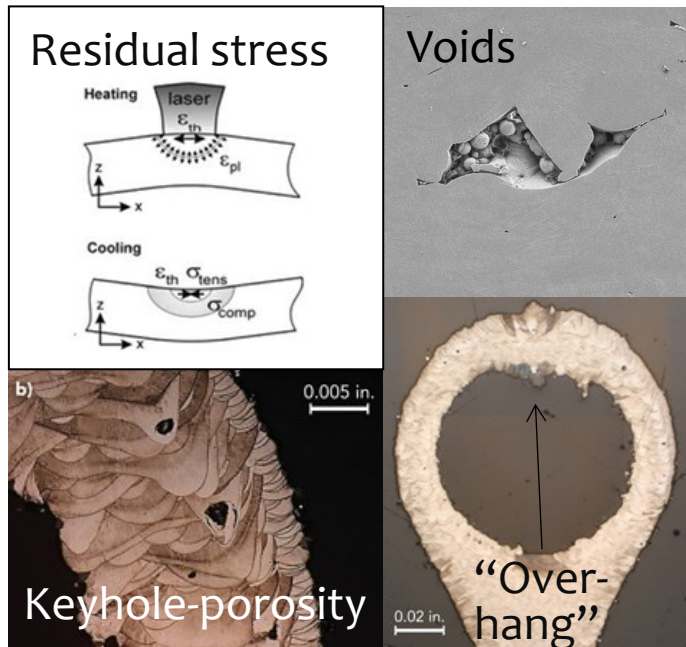


Metal additive manufacturing based on Selective Laser Melting of powders has greatly enabled design flexibility



LLNL efforts in this area aimed at modeling and qualification of SLM, process monitoring, and **improved model validation**

Despite apparent simplicity of technique, multiple physical phenomena govern SLM



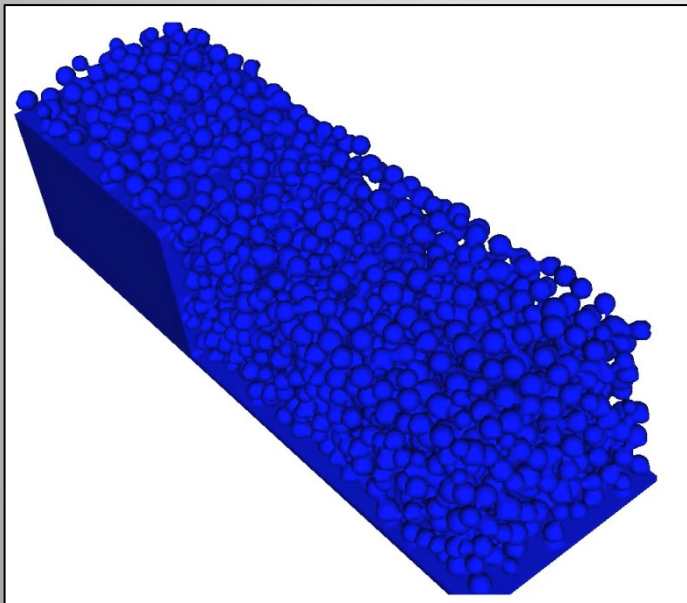
A red arrow points from the list of physical phenomena to the micrographs of voids and keyhole-porosity.

- Absorption
- Vaporization
- Capillarity
- Hydrodynamics
- Marangoni Convection
- Wetting/dewetting
- Phase transformation
- Phase separation
- Convection
- Radiation
- ...

Experimentally probing the laser melting process *in situ* can yield insight to these multiple physical effects

Model-driven experimentation is sought to minimize defects which can limit AM performance

Laser powder melt simulation



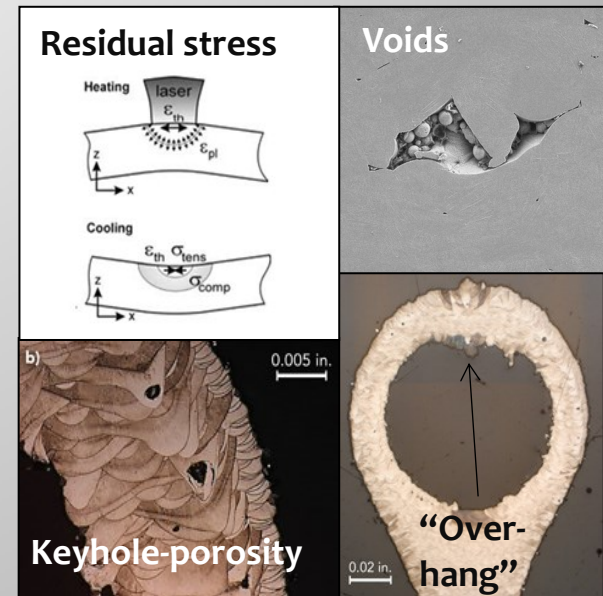
S. Khairallah and A. Anderson

Physics

Absorption
Vaporization
Capillarity
Hydrodynamics
Marangoni
Convection
Wetting/dewetting
Phase transformation
Phase separation
Convection
Radiation
...



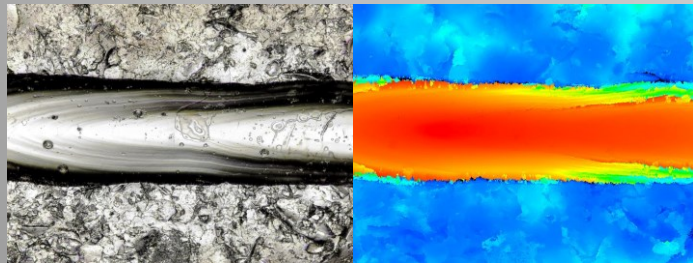
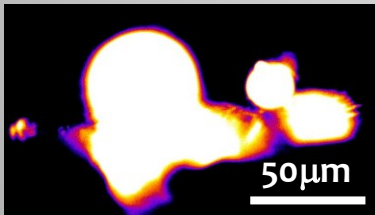
Defects



Goals

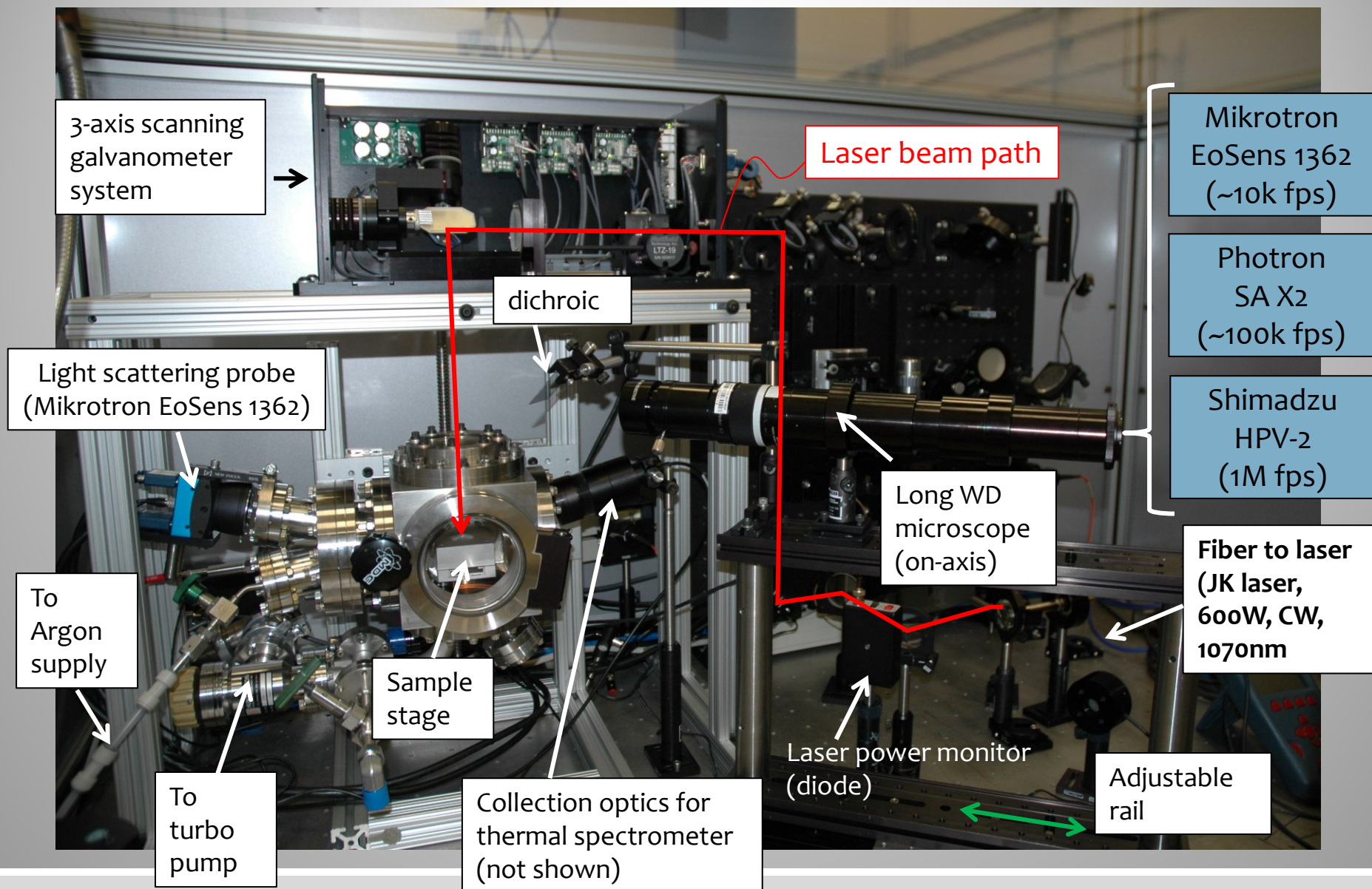
- Demonstrate high speed, microscopic technique to directly probe heating, melting and wetting of metal powders used in SLM
 - Extend to higher effective scan rates, higher powers & higher frame rates
- Compare to simulations to improve understanding of SLM process, validate models

Approach



- Use high frame-rate CMOS camera microscopy to image single layer, metal particle bed melting under varying laser and environmental conditions
- Use self-illumination incandescence from heated particle to characterize melt pool dimensions, particle/splash ejection
- Compare thermal emission history with final material deposition morphologies

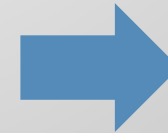
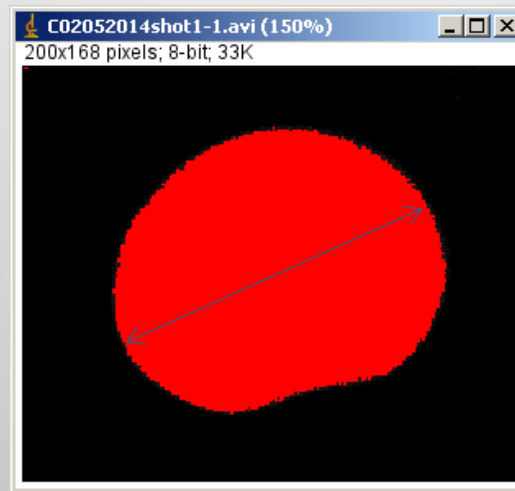
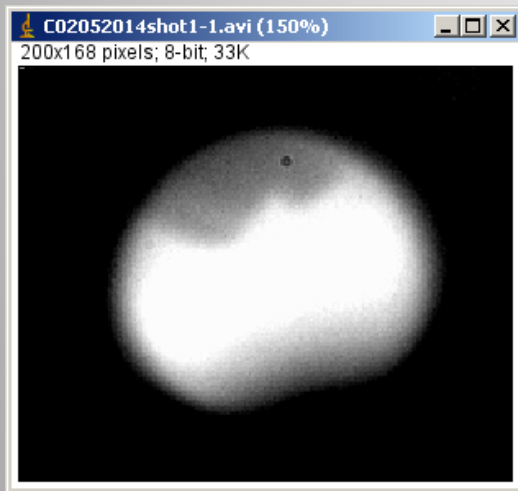
Experimental setup



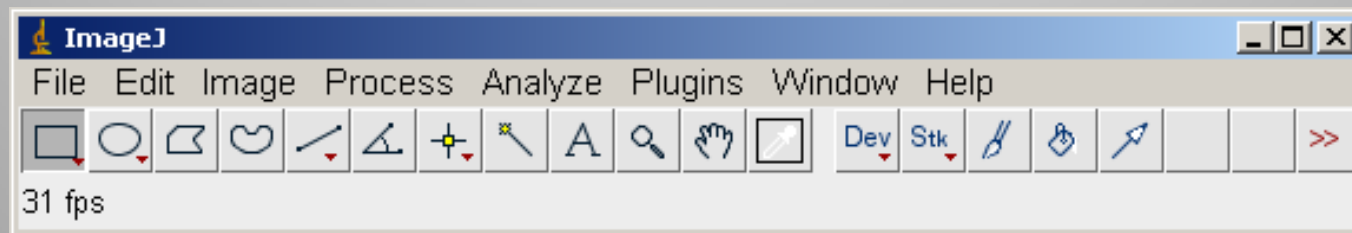
Analysis of single particle shape evolution from high speed image files

Raw 8-bit image
(10kHz, 200x168pix)

Threshold mask (25-255)

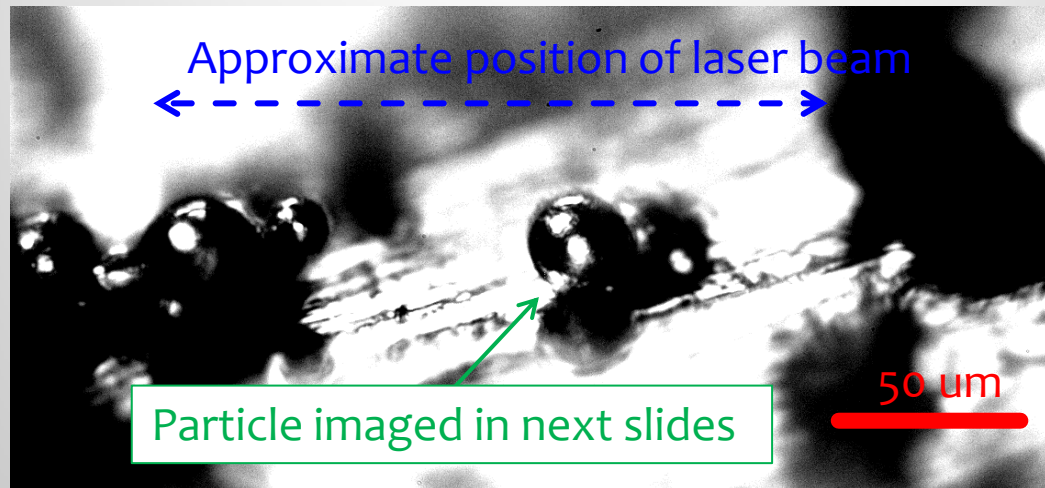


Feret's diameter
Area
Circularity
Center of mass
Intensity
...



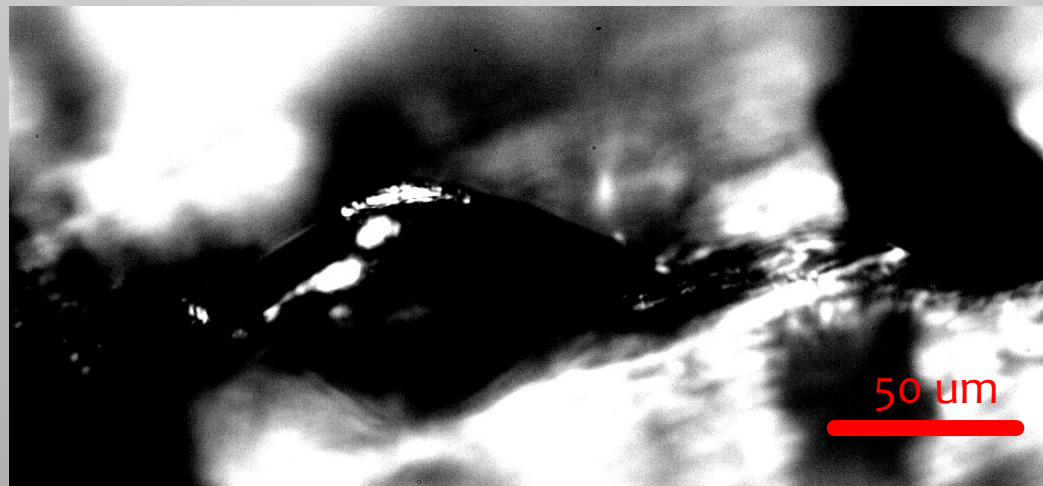
Initial and final morphology of laser-induced melting of sparse 316L layer

Pre-shot



5~50 W of 10.6 μm light into 200 μm ($1/e^2$), $\tau=50$ ms

Post-shot



10 kHz imaging of laser-generated incandescence (total movie time 70 ms)

Thermo-isolated heating time:

$$\alpha \pi R I \tau = 4/3 \pi R^3 \rho C T_m$$

$$\tau_{\text{HC}} \sim 4/3 R \rho C T_m / \alpha I \sim \underline{0.75 \text{ ms}}$$

Thermal conduction time:

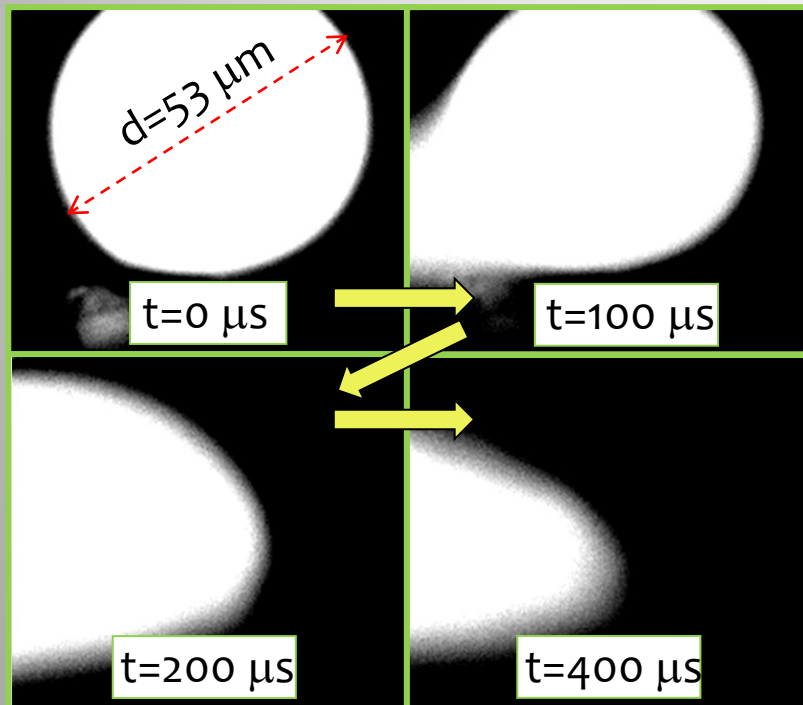
$$\tau_c \sim R^2 / D, D = 0.04 \text{ cm}^2/\text{sec}$$

for $R = 15 \text{ } \mu\text{m}$ steel particles:

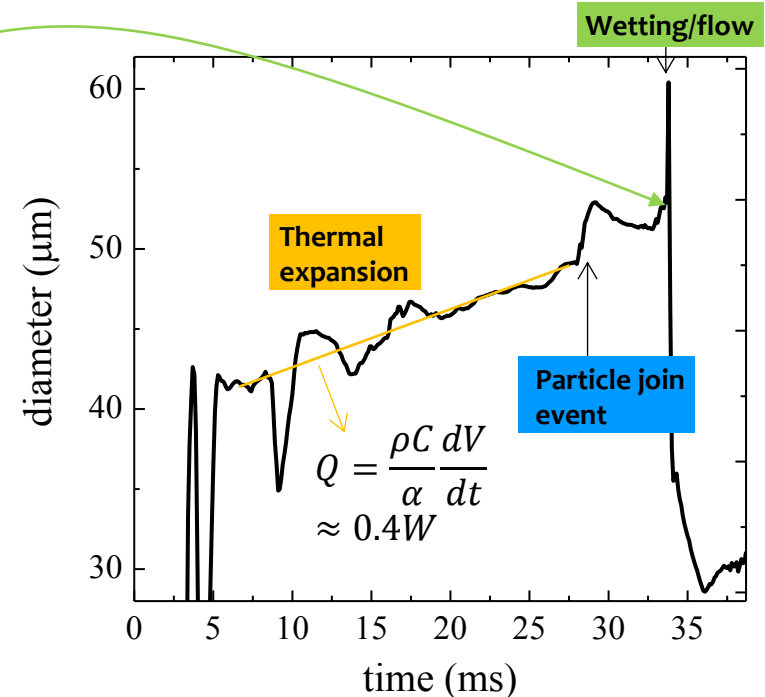
$$\underline{\tau_c = 56 \text{ } \mu\text{s}}$$



Dynamics of steel 316L particle was irradiated with IR laser light was revealed using 10k fps imaging



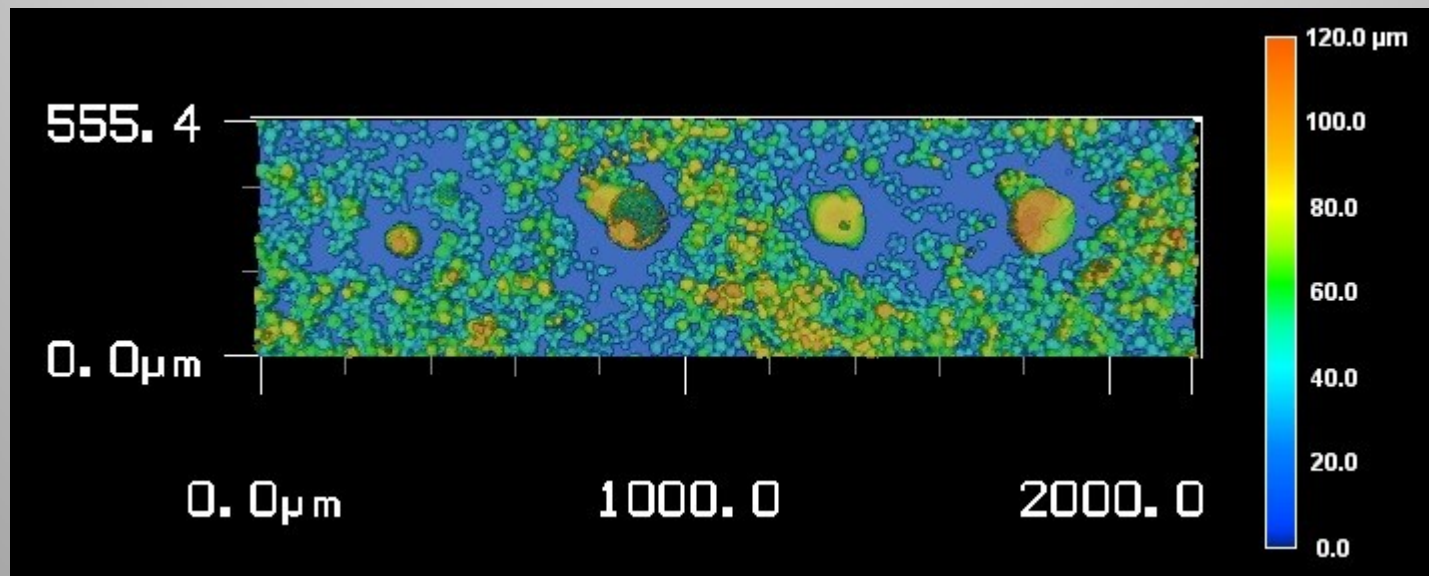
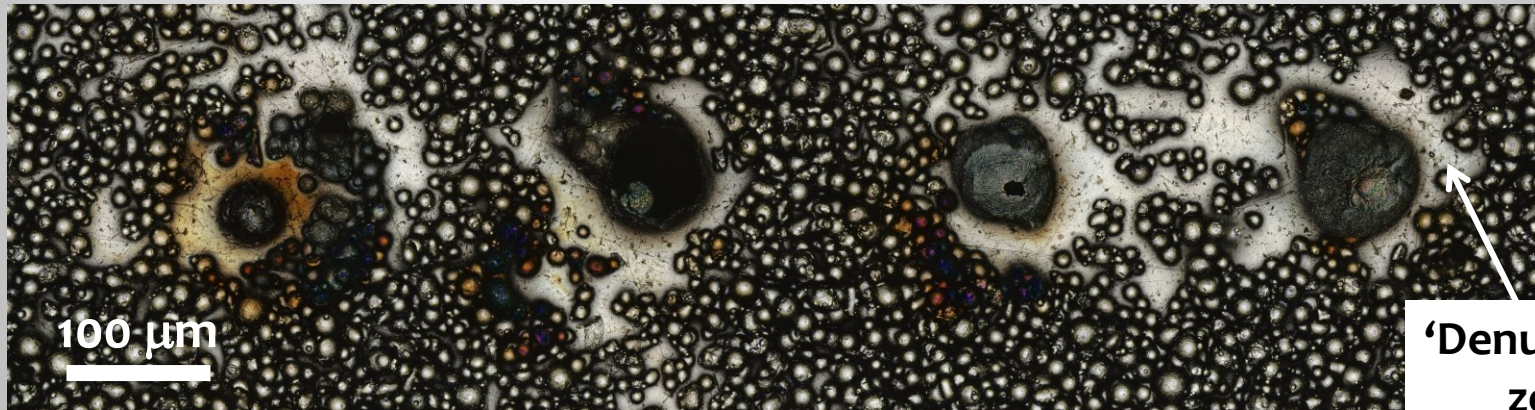
Measured particle dynamics captures expansion, melting & wetting



~4 ms delay observed between melting and wetting indicates highly non-uniform heat distribution

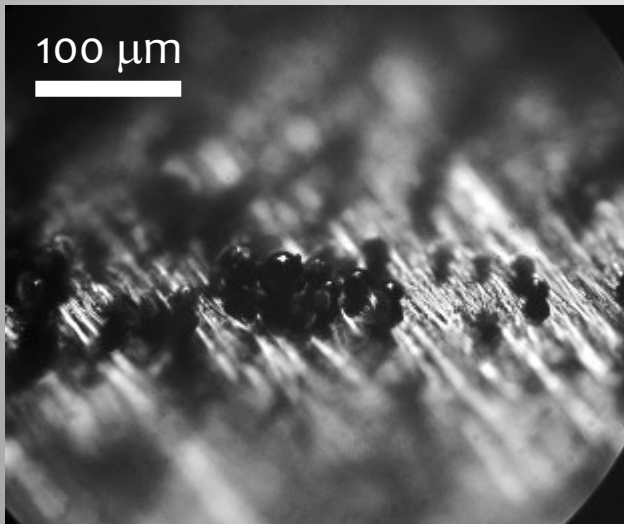
Single layer of SS 316L powder exposed to single ~10W pulses shows conglomeration and denudation effects

Laser
spot
size:
~80 μm

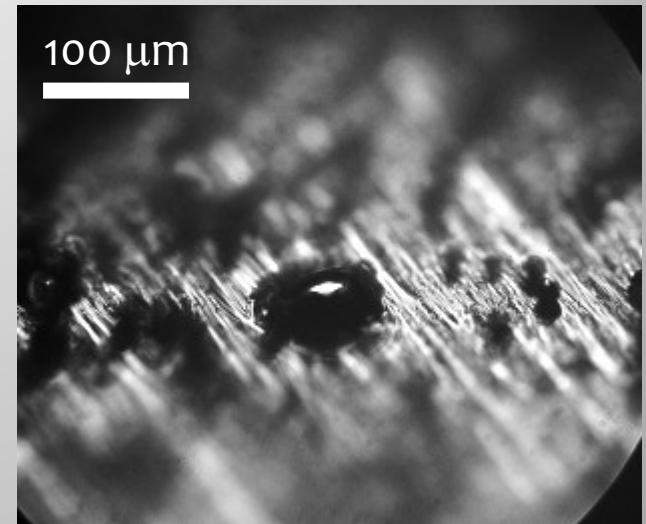


**Steel 316L particle cluster irradiated with 100W , $50\mu\text{m}$ $1/e^2$
Gaussian diameter beam: 1Mfps , $15\mu\text{s}$ start delay, 100 frames total**

before

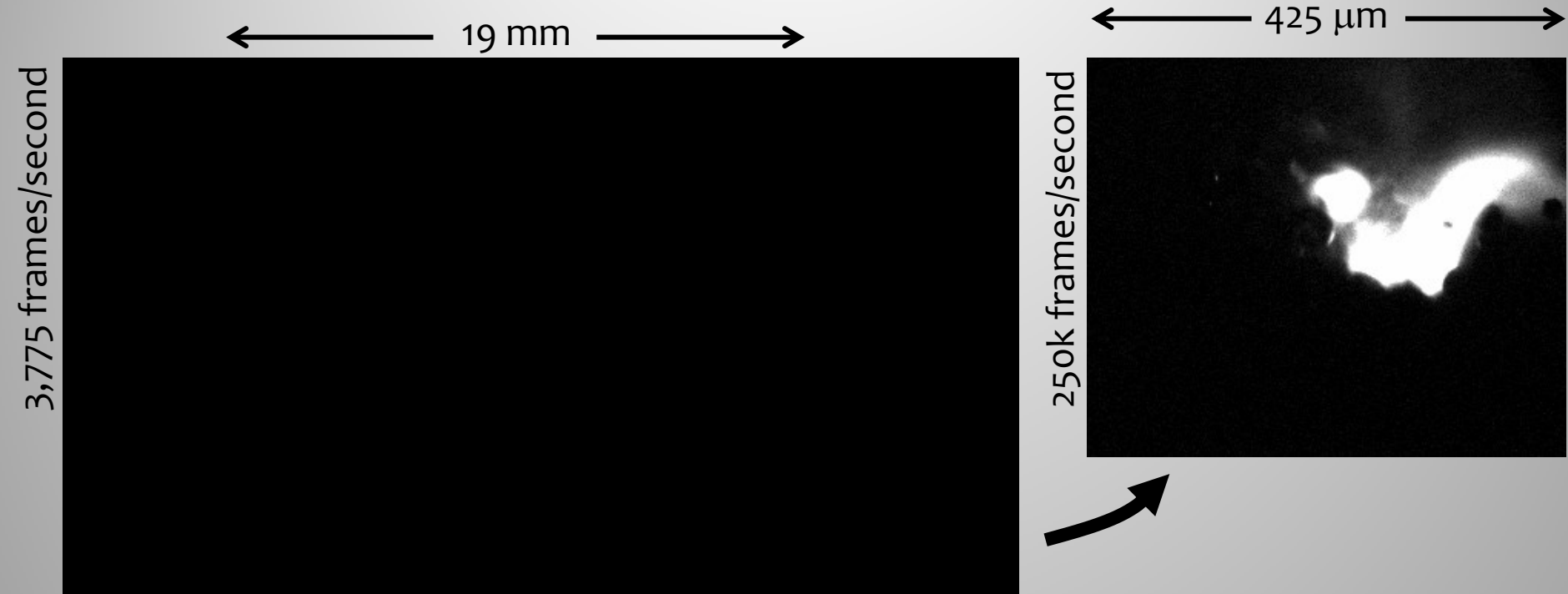


after

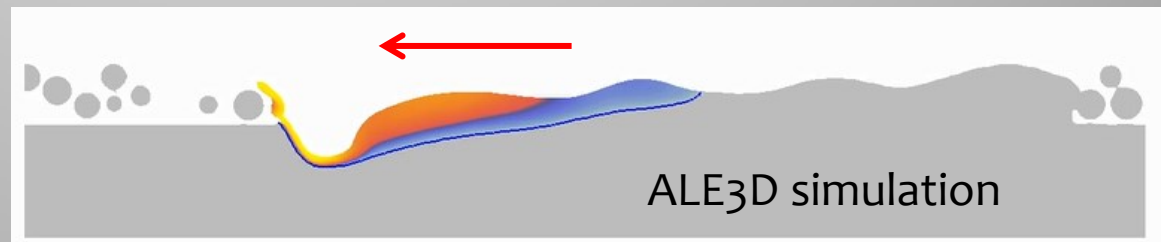


- Apparent lack of wetting
- Fluid wave speeds $\sim 10\text{-}17\text{ m/s}$
- Droplet ejection at 12.6 m/s

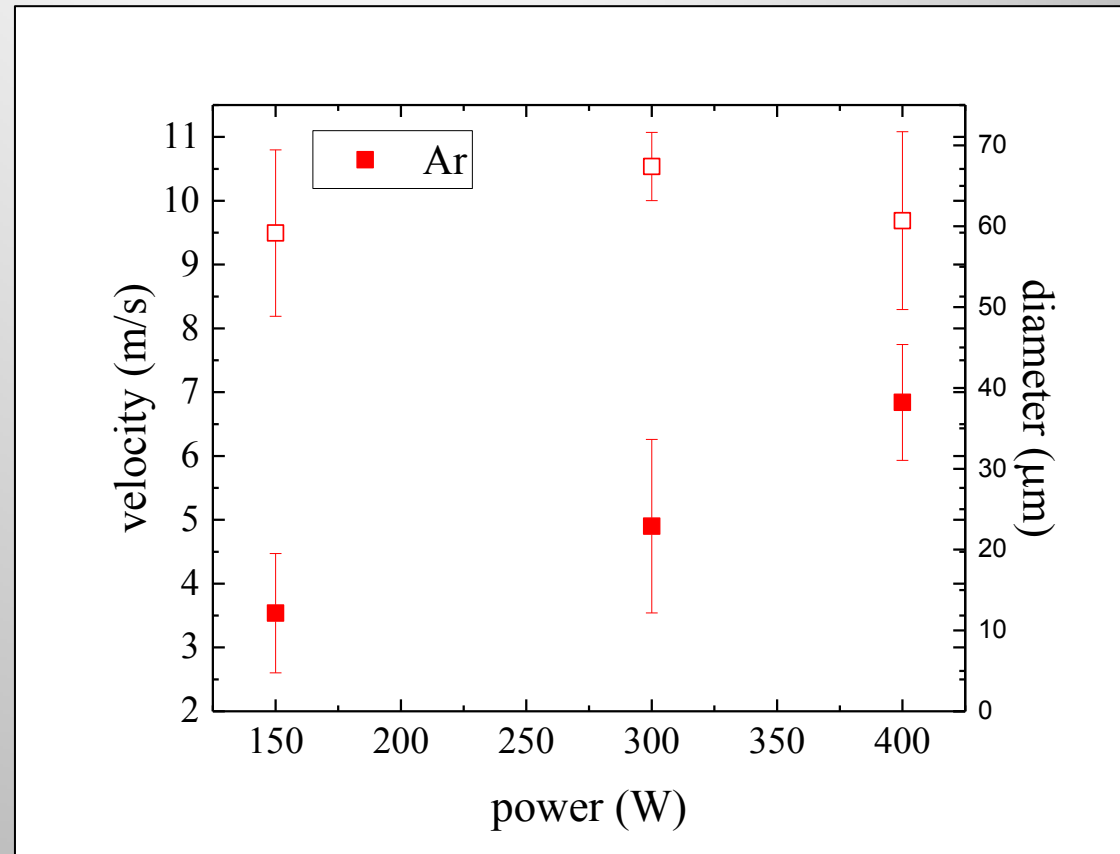
Off-axis imaging of molten particle ejection with scanning beam ($P=150\text{W}$, $a=50\mu\text{m}$, $u=500\text{ mm/s}$)



Evaporation-driven recoil momentum shapes melt track, ejects material



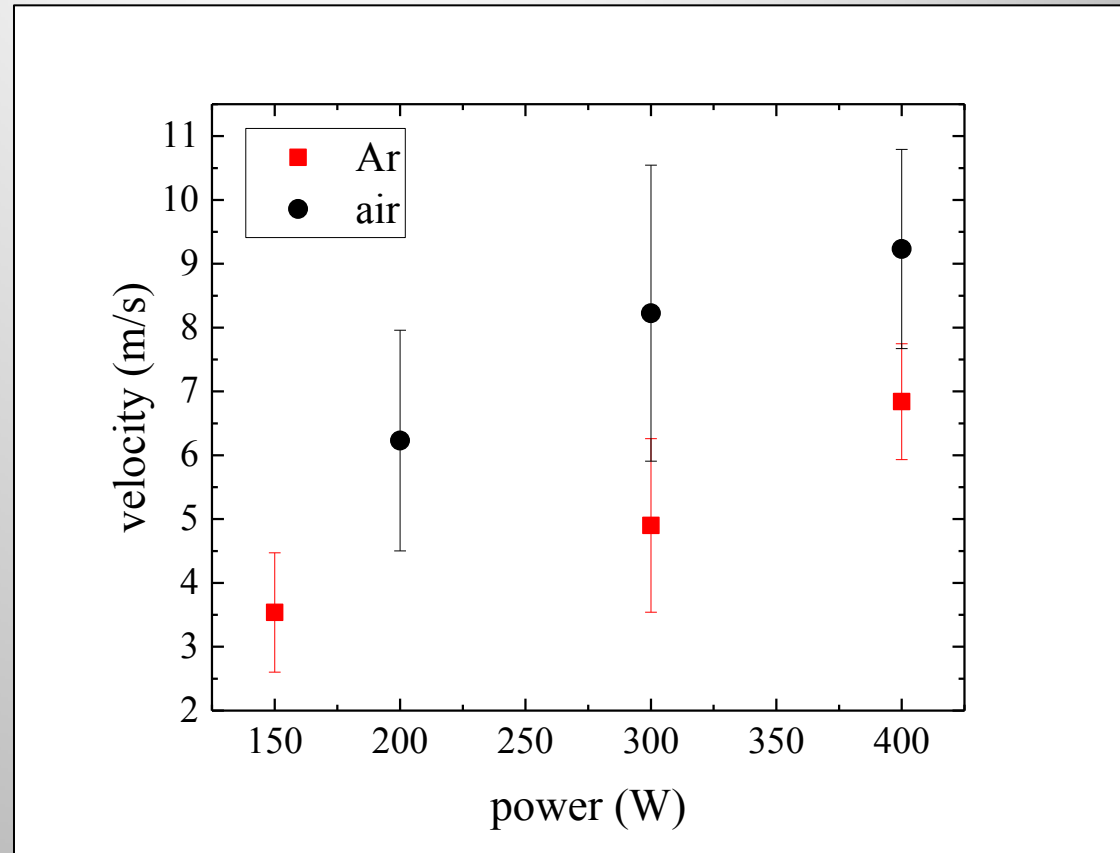
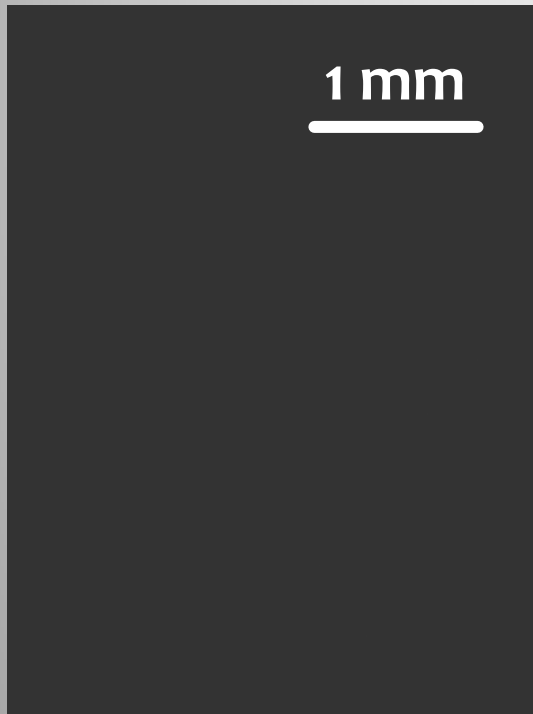
Measured ejection velocities and particle sizes as a function of laser power (1200 mm/s scan speed)



- Velocity increases with laser power due to increased recoil pressure
- Droplet size did not vary appreciably with laser power

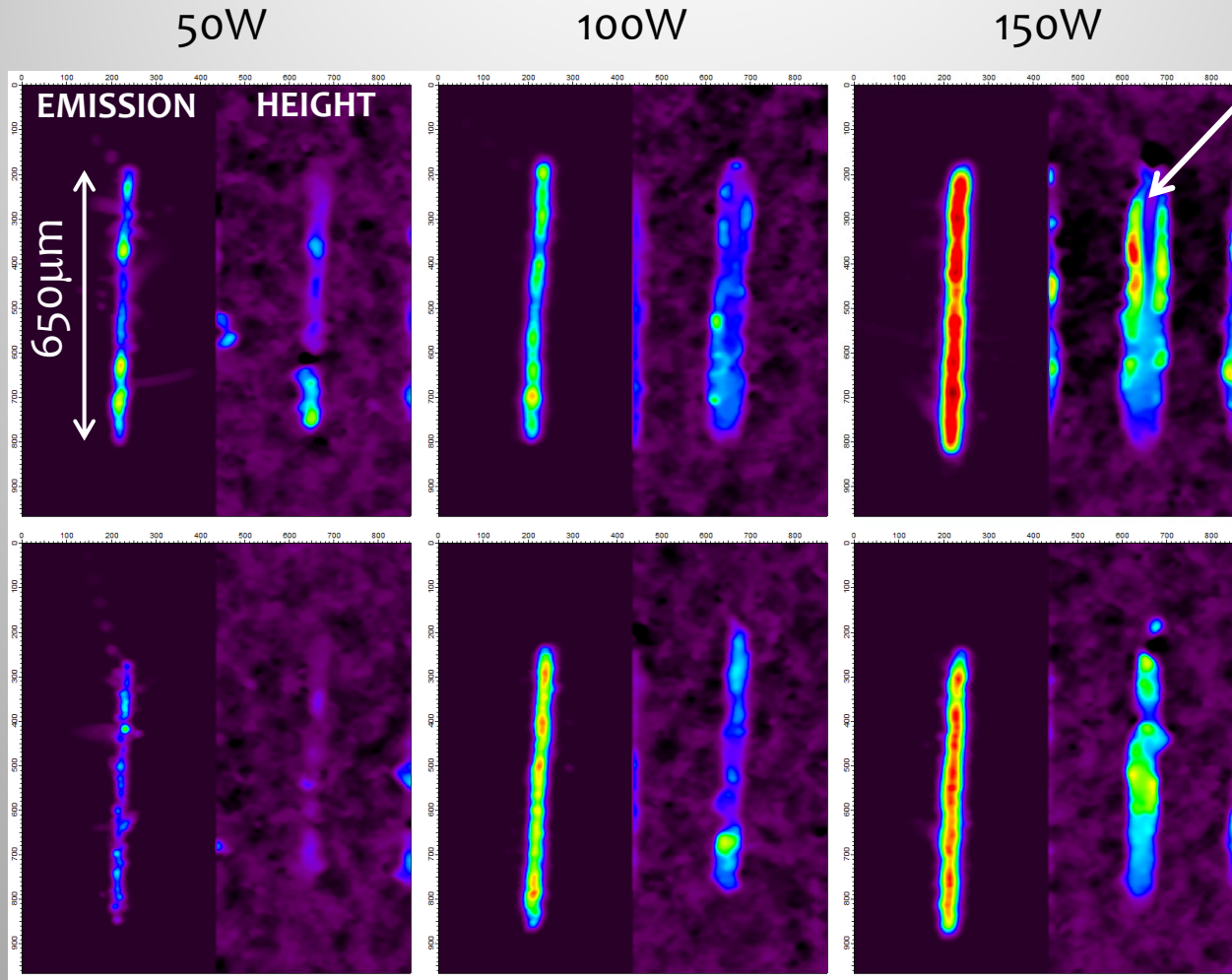
Measured ejection velocities as a function of laser power (1200 mm/s scan speed): effect of oxidation

150W, 1200 mm/s

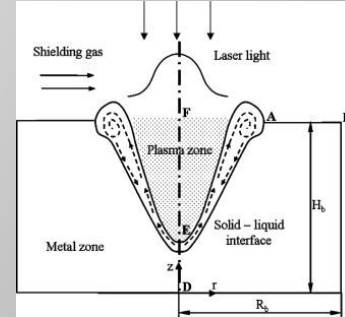


- Oxidation leads to increased heating, pressure
- Droplet size not affected by oxidation ($\sim 70\mu\text{m}$, not shown)

Comparison of thermal emission history and final deposited material morphology

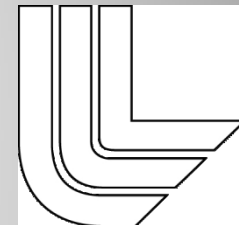


“keyholing”



Summary

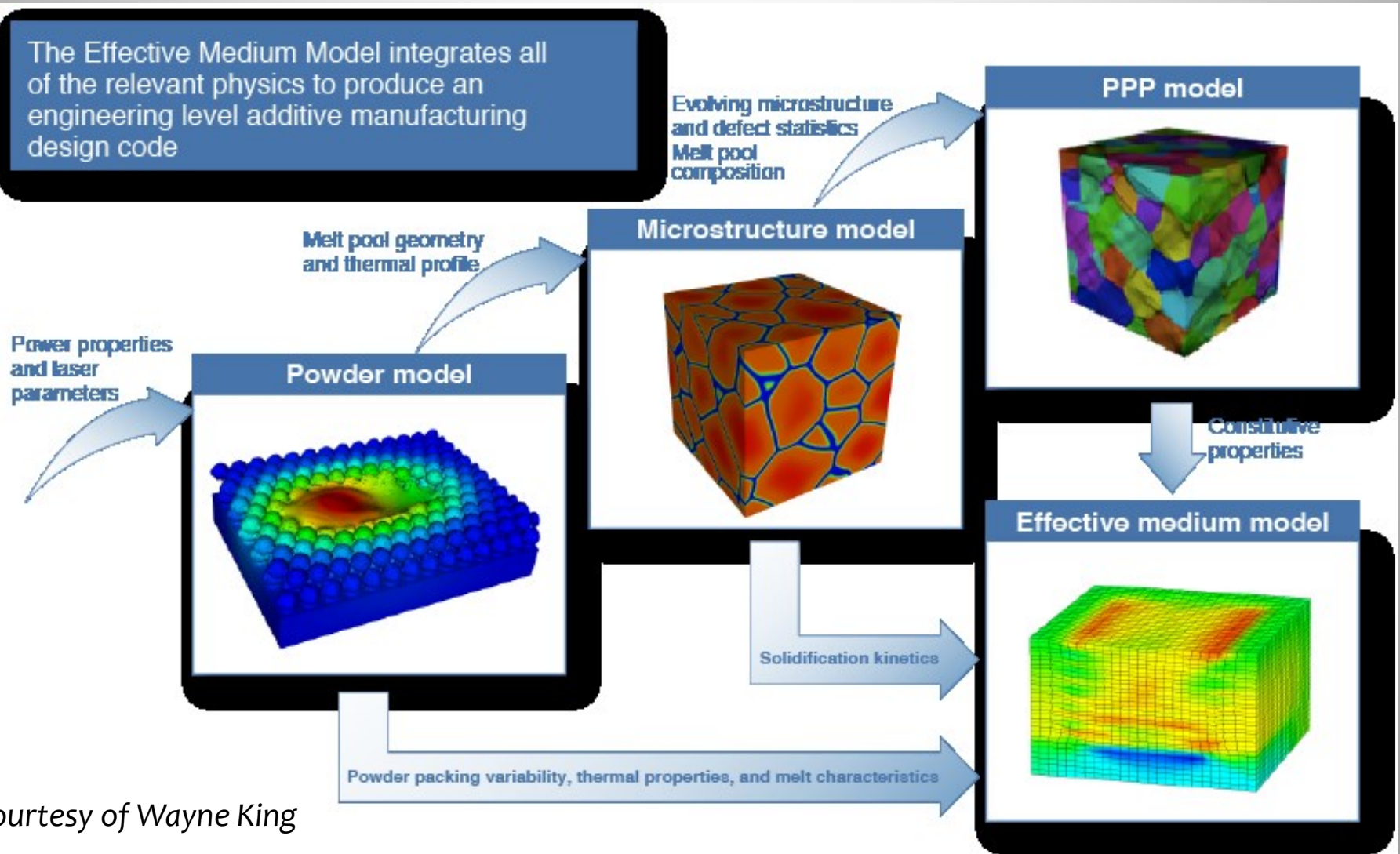
- An imaging test bench to monitor dynamic of laser-induced melting of stainless steel powders using high frame rate (up to 1 MHz) imaging was demonstrated
- Keyholing from evaporation-driven recoil pressure was observed at high laser power, with a threshold in agreement with reported predictions
- Delayed/frustrated wetting was observed, which could lead to large fluctuations and instability in droplet diameters
- Ejection velocities for typical SLM deposition conditions were on the order of 3-7 m/s, increasing with laser power and oxygen content
- Future work will include pulsed laser illumination and full 3D build temperature monitoring



THANK YOU FOR YOUR ATTENTION!



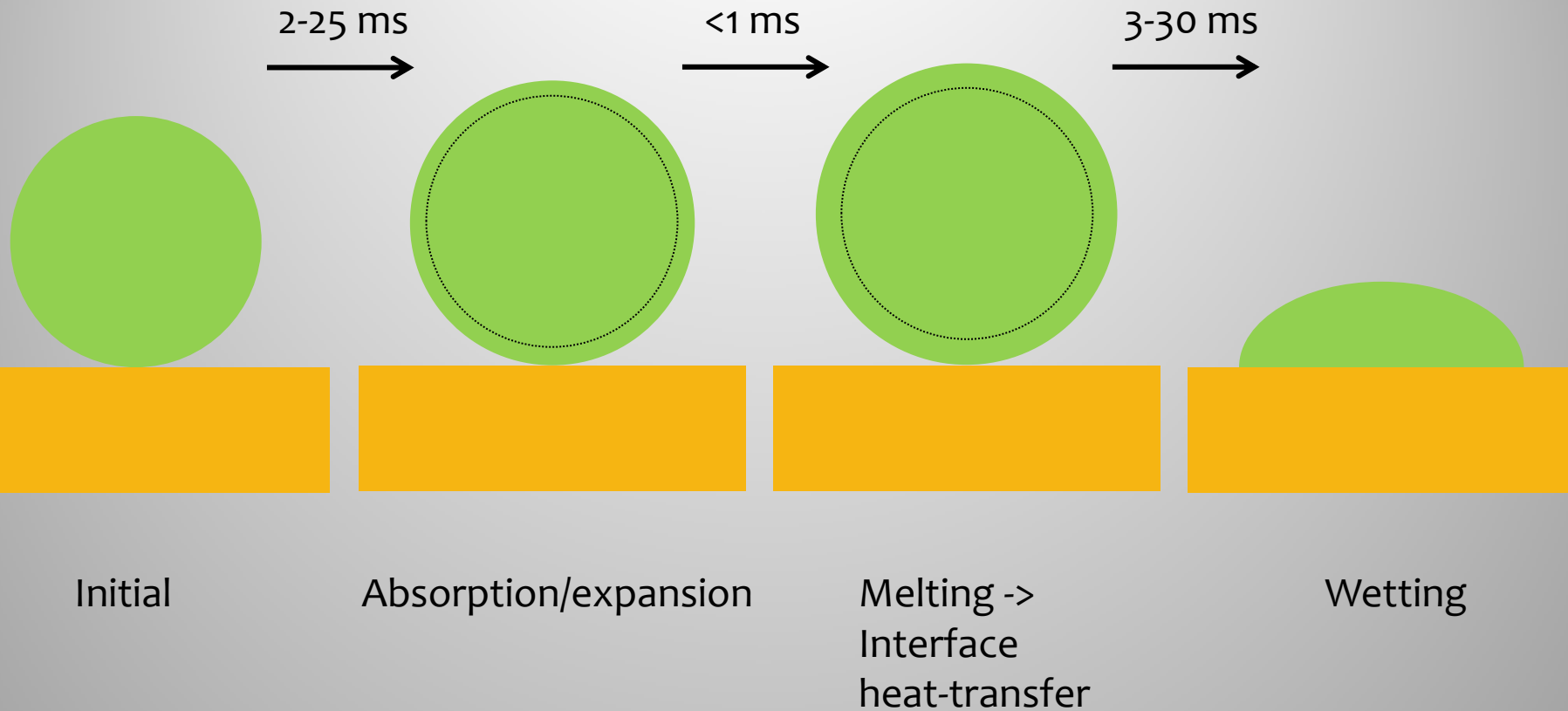
High performance computing is being leveraged to Accelerate Qualification of Additive Manufactured parts



Courtesy of Wayne King



Analysis of melt-wetting dynamics



Estimating melt times and particle-substrate heat transfer under laser irradiation

Absorptivity for polished stainless steel at $\lambda=10.6 \mu\text{m}$ is ~ 0.1

For the underlying substrate, with thermal conductivity the value near the melting point is $k=36 \text{ W/m.K} \rightarrow T \sim 112 \text{ C}$ (won't melt substrate!)

Thermal conduction time: $\tau_c \sim R^2/D$, $D=0.04 \text{ cm}^2/\text{sec}$ for SS, $R=15 \mu\text{m}$
 $\tau_c = 56 \mu\text{s}$

Thermo-isolated heating time: $\alpha \pi R I \tau = 4/3 \pi R^3 \rho C T_m$
 $\tau_{\text{Hc}} \sim 4/3 R \rho C T_m / \alpha I \sim \underline{0.75 \text{ ms}}$

However, finite element simulations of a particle in thermal contact with the substrate, $\tau_{\text{Hc}} < 20 \text{ ms}$

Wetting time: Laplace pressure + Bernoulli Eq. $\rightarrow 1\text{-}10 \mu\text{s}$